SOURCE TEST REPORT

17-340

CONDUCTED AT

Carlton Forge Works

7743 Adams Street Paramount, CA 90723

HEXAVALENT CHROMIUM EMISSIONS FROM FURNACE #431

TESTED:

May 18, 2017

ISSUED:

September 1, 2017

REPORTED BY:

P. Eric Padilla

Air Quality Engineer II

REVIEWED BY:

Michael Garibay

Supervising Air Quality Engineer

SOURCE TEST ENGINEERING BRANCH

MONITORING & ANALYSIS DIVISION

Test No. <u>17-340</u> 2 Date: <u>5/18/2017</u>

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SUMMARY

a.	Firm	Carlton Forge Works
b.	Test Location	7743 Adams Street, Paramount, CA 90723
c.	Unit(s) Tested	Furnace #431
d.	Test Required by	Matt Miyasato, PhD (SCAQMD DEO), (909)396-3249
e.	Reason for Test Request	High ambient monitor readings of Cr (VI)
f.	Date of Test	May 18, 2017
g.	Source Test Performed by	Jason Aspell, Eric Padilla
h.	Test Arrangements Made Through	Armando Bautista (Environmental Manager, Carlton Forge Works) (562) 633-1131
i.	Source Test Observed by	Armando Bautista, James Wright (Division – Environmental Manager, Wyman-Gordon)
j.	Company Facility I.D.	22911
k.	Permit/Application Number	N/A

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EXECUTIVE SUMMARY

Due to ongoing citizen odor complaints regarding Carlton Forge Works and allegations that elevated nearby monitoring results were related to these complaints, Source Test engineers from the SCAQMD Source Test Branch conducted screening source testing on May 18, 2017 on Furnace #431 to determine hexavalent chromium emissions from the furnace. The testing resulted in hexavalent chromium emissions that were higher than the average ambient monitor readings in the days surrounding the test date, but on the lower end of the range of other furnace emissions that have been tested by the SCAQMD.

Summary of Test Conditions

During the source test, Furnace #431 was operating at approximately 1900° F. The parts within the furnace were Waspaloy®, which contains approximately 18% chromium. Because of the nature and configuration of the process, testing was performed non-isokinetically, as a screening test, due to the lack of sample ports or a stack to determine exhaust rate. The results are listed in Table 1. The emissions are expressed in nanograms per cubic meter (ng/m³) for the source test as well as the ambient monitors.

Four ambient monitors are located near the Carlton Forgeworks facility. Figure 1 displays the locations of the monitors in relation to the facility (circled). Monitors #2 and #28 are just east of the plant site and monitors #3 and #25 are further east, on or near the premises of Lincoln Elementary School. Results from the ambient monitors in the timeframe near the time of the test are shown in Table 2.

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RESULTS

Below are the emissions from Furnace #431 (Table 1) and ambient air monitoring data for four monitors near the Carlton Forge Works facility. For locations of the monitors relative to the facility, see Figure 1.

Table 1 – Hexavalent Chromium Emissions May 18, 2017

Emissions Source	Concentration (ng/m³)
Furnace #431	137

Table 2 – Air Monitoring Data for the Area Near Carlton Forge Works (ng/m³)

Monitor	May 10, 2017	May 13, 2017	May 16, 2017	May 19, 2017
2 (SE of facility)	0.12	0.03	0.18	0.32
3 (NE of facility)		0.56		0.17
25 (E of facility)	2.60	0.43	0.16	0.53
28 (NE of facility)	1.87	0.18		0.62

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INTRODUCTION

On May 18, 2017, Source Test Engineers from the South Coast Air Quality Management District (SCAQMD) Source Test Engineering Branch conducted source testing on Forging Furnace #431 at Carlton Forge Works in Paramount, CA. The purpose of the testing was to attempt to identify the source of elevated ambient hexavalent chromium levels measured near the facility.

Carlton Forge Works is a producer of open and closed die forged products primarily for the aerospace industry. The facility mainly forges billets from exotic metals to specific shapes and rolled rings. Testing was performed to determine hexavalent chromium in the exhaust from one of the forging furnaces, Furnace #431.

EQUIPMENT & PROCESS DESCRIPTION

Billets are heated in forge furnaces until they reach the desired temperature. They are removed from the furnace and subjected to mechanical molding from presses, dies, and rollers. The process is repeated as necessary to cause the part to conform to the specified requirements. Throughout processing (pre-, during, and post-forming), parts may be subjected to grinding to eliminate defects. Testing for this source test was restricted to the furnace operations.

Furnace #431 contained parts composed of Waspaloy®, which contains approximately 18% chromium. At the time of the testing, the furnace was running at approximately 1900° F.

The refractory in the furnace was last re-bricked on February 17, 2016.

During testing, the furnace damper opened and closed slightly. The pressure within the furnace was +0.06 inches H₂O.

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SAMPLING & ANALYTICAL PROCEDURES

General

One sampling train was utilized for a non-isokinetic screening test. Sampling was performed using train #50. Train #49 was retained as a blank sample.

Sampling was performed with the probe arranged at the opening of the damper to the furnace in such a way that it would not be damaged or interfere with the operation of the damper (see Figure 2). There was no sampling stack.

Hexavalent Chromium Sampling

Testing was conducted based on California Air Resources Board Method 425 applied to the furnace exhaust, with the procedures of the method specific to stack sampling omitted because the furnace does not have a stack conducive to isokinetic sampling. One sample was taken at a single non-isokinetic sample point as described above for informational purposes. A second sampling train was used as a blank sample, without a probe or tubing. The furnace sampling train consisted of a quartz probe and teflon sampling line, which was used to draw the stack sample from the source. The sample was then drawn through two impingers each filled with an aqueous solution of 0.1N NaHCO₃ (per Section 21.2 of the Method), an empty impinger, a 2" glass filter, and an impinger filled with tared silica gel. The sampling train was connected to a leak free vacuum pump, a dry gas meter, and a calibrated orifice. The impingers were contained in an ice bath to condense water vapor and other condensable matter present in the sample stream (see Figure 2).

The samples were collected from the exhaust stream using the sampling train. The pH of the solution in the first impinger was measured after the test, but prior to recovery, at pH of at least 9 (the method requires a pH of 8.0 or higher). The impinger solutions were recovered within 24 hours and the SCAQMD laboratory analyzed the hexavalent chromium in the samples by CARB Method 425. Hexavalent chromium deposited in the filter, sample line and impingers were extracted and analyzed by an Ion Chromatograph equipped with a post-column reactor (IC/PCR) and a visible wavelength detector. Moisture content was determined gravimetrically and volumetrically.

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DISCUSSION/TEST CRITIQUE

The samples were not taken isokinetically because the stack was not conducive to isokinetic sampling on the furnace. The exhaust was extracted at a constant rate and the total volume of the sample was used to determine the mass emissions of the furnace exhaust. More precisely representative emissions samples would require a portable stack or other method for sampling isokinetically. The purpose of the screening samples are to identify potential sources of high hexavalent chromium levels so that further testing may be conducted, if necessary.

To more effectively interpret the test results, the results of the most recent Multiple Air Toxics Exposure Study (MATES), MATES IV, conducted by SCAQMD, should be considered. In that study, the typical ambient level of hexavalent chromium in the Los Angeles Basin averaged 0.06 ng/m³. The emissions from Furnace #431, which were 137 ng/m³, were orders of magnitude higher than this average. Though it should be noted that levels of source emissions are reduced over distance as dilution occurs, the elevated levels at the ambient monitors indicate that high levels of hexavalent chrome are being emitted in Paramount. The furnace testing indicates that Furnace #431 potentially contributes to the high ambient readings.

As of the issue date of this report, SCAQMD has measured a wide variation of furnace emissions concentrations from 19 to 24,400 ng/m³. Although the emissions from Furnace #431 are on the lower end of the range and may not have a large impact on the ambient monitoring readings, it is thought that the overall effect of the numerous furnaces emitting at various emissions levels at the facility may individually and/or cumulatively have a significant effect on the measured ambient concentrations.

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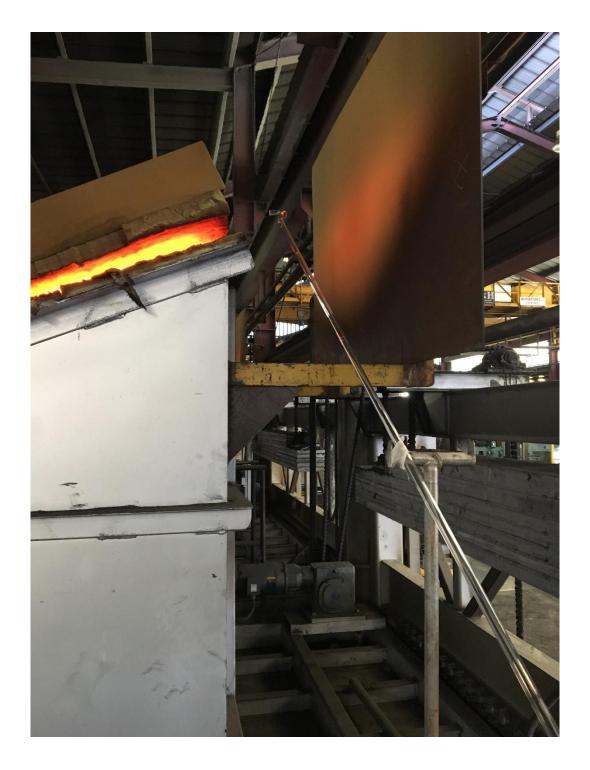
FIGURES

Figure 1: Air Monitor Map



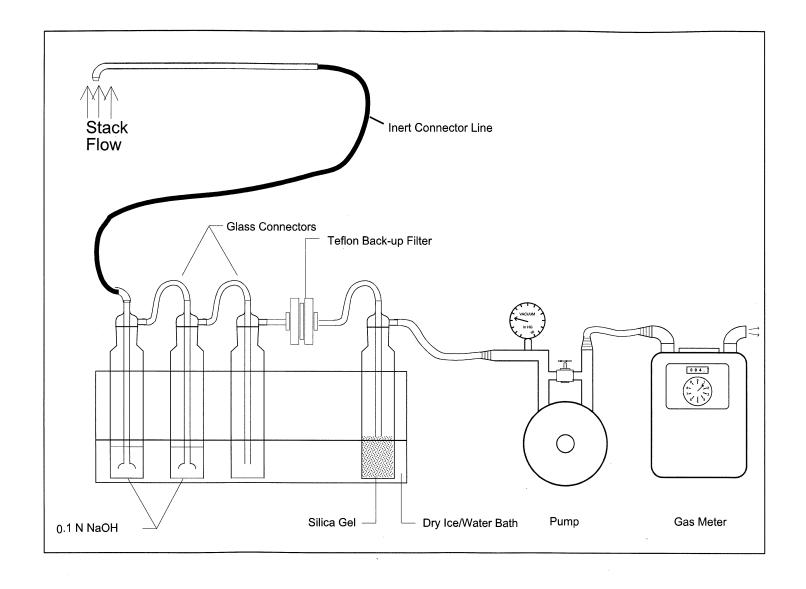
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Figure 2: Sampling Probe Placement



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Figure 3: CARB Method 425 Train Diagram



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CALCULATIONS

Test N	lo. 1					Test Date:	3/29/17	
		SOU	RCE TEST	CALCULATIONS	 3			
Sampling Location:	Mattco For	rge - Grinding	Area					
Sample Train:	11	gg				Input by:	E. Padilla	
SUMMARY								
A. Average Traverse V								fps
B. Gas Meter Tempera								deg F
C. Gas Meter CorrectionD. Average Orifice Pre								"H ₂ 0
E. Nozzle Diameter								inch
E. Hollio Diamotoriii.							***********	IIICII
F1. Stack Diameter or	Dimension #1		inch	M. Pitot Correct	tion Facto	or	0.84	
F2. Stack Dim #2 (blan				N. Sampling Tir				min
G. Stack Cross Sect. A				O. Nozzle X-Se				
H. Average Stack Tem			deg F	P. Net Hex Chro				•
 Barometric Pressure Gas Meter Pressure 				Q. Hex Chrome R. Water Vapor				-
K. Static Pressure			ngA "H₂0	S. Gas Volume				
L. Total Stack Pressure				S2. Amp-hr				amp-hr
						*		
U. Percent Water Vap	or in Gas Sam	ple ((4.64 x R	R)/((0.0464 >	(R) + T))			1.47	%
PERCENT MOISTURE U. Percent Water Vap V. Average Molecular Component	or in Gas Sam Weight (Wet)	ple ((4.64 x R			Molecu			% t./Mole
U. Percent Water Vapo V. Average Molecular Component Water	or in Gas Sam Weight (Wet) V	iple ((4.64 x R			Molecu 18.0			
U. Percent Water Vapo V. Average Molecular Component 	or in Gas Sam Weight (Wet) V	pple ((4.64 x R : ol. Fract. x Dry Basis	Moist. F		Molecu 18.0 44.0		= W	
U. Percent Water Vape V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide	Weight (Wet) V 0.015 0.00040	pple ((4.64 x R : ol. Fract. x Dry Basis Dry Basis	Moist. F		Molecu 18.0 44.0 28.0		= W 0.27 0.02 0.00	
U. Percent Water Vapor V. Average Molecular Component	v (Weight (Wet) V 0.015 0.00040 0.20900	ol. Fract. x Dry Basis Dry Basis Dry Basis	1.000 0.985 0.985 0.985		18.0 44.0 28.0 32.0		= VV 0.27 0.02 0.00 6.59	
U. Percent Water Vape V. Average Molecular Component	v (Weight (Wet) V 0.015 0.00040 0.20900	pple ((4.64 x R : ol. Fract. x Dry Basis Dry Basis	Moist. F		Molecu 18.0 44.0 28.0		= W 0.27 0.02 0.00	
U. Percent Water Vape V. Average Molecular Component	v (Weight (Wet) V 0.015 0.00040 0.20900	ol. Fract. x Dry Basis Dry Basis Dry Basis	1.000 0.985 0.985 0.985		18.0 44.0 28.0 32.0		= VV 0.27 0.02 0.00 6.59	
U. Percent Water Vape V. Average Molecular Component	v (Weight (Wet) V 0.015 0.00040 0.20900	ol. Fract. x Dry Basis Dry Basis Dry Basis	1.000 0.985 0.985 0.985		18.0 44.0 28.0 32.0	, , , , , , , , , , , , , , , , , , ,	= W 0.27 0.02 0.00 6.59 21.97	
U. Percent Water Vape V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts	0.015 0.00040 0.20900 0.791	ol. Fract. x Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis	1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , , Sum	= W 0.27 0.02 0.00 6.59 21.97	
U. Percent Water Vape V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct	Veight (Wet) V 0.015 0.00040 0.20900 0.791	ol. Fract. x Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84	
U. Percent Water Vapo V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C	V 0.015 0.00040 0.20900 0.791	ol. Fract. x Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis Ory Basis Ory Basis Ory Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84	
U. Percent Water Vapo V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x 6	Weight (Wet) 0.015 0.00040 0.20900 0.791 ction Factor (2 orrection Fact A x M x W x X	Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis Ory Basis Ory Basis Ory Basis Ory Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84	fps cfm
U. Percent Water Vapo V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x 6 AA. Flow Rate (Standa)	0.015 0.0040 0.20900 0.791 ction Factor (2 orrection Fact A x M x W x X S0)	Dry Basis Ory Basis Ory Basis Ory Basis Ory Basis	Moist. F. 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0!	fps cfm scfm
U. Percent Water Vape V. Average Molecular Component	0.015 0.0040 0.20900 0.791 ction Factor (2 orrection Fact A x M x W x X S0)	Dry Basis Ory Basis Ory Basis Ory Basis Ory Basis	Moist. F. 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0!	fps cfm scfm
U. Percent Water Vapor V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x 6 AA. Flow Rate (Standa) BB. Dry Flow Rate (AA	Veight (Wet) V 0.015 0.00040 0.20900 0.791 etion Factor (2 correction Fact A x M x W x X S0)	Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis Ory Basis Ory Basis Ory Basis Ory Basis Ory Basis Ory Basis	Moist. F. 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0!	fps cfm scfm
U. Percent Water Vapo V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x 6 AA. Flow Rate (Standal BB. Dry Flow Rate (AA	0.015 0.00040 0.20900 0.791 ction Factor (2 orrection Factor (2 o	Dry Basis Ory Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0! #DIV/0!	fps cfm scfm dscfm
U. Percent Water Vapor V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x 6 AA. Flow Rate (Standa) BB. Dry Flow Rate (AA	vition Factor (2 orrection	Dry Basis Ory Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	Molecu 18.0 44.0 28.0 32.0 28.2	, , , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0! 5.992E-08	fps cfm scfm dscfm
U. Percent Water Vapo V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x 6 AA. Flow Rate (Standal BB. Dry Flow Rate (AA SAMPLE CONCENTRA CC. Sample Concentra	vition Factor (2 orrection Factor A x M x W x X (50)	Dry Basis Ory Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	Molecu 18.0 44.0 28.0 32.0 28.2	llar Wt.	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0! #DIV/0! 5.992E-08 3.24E-05	fps cfm scfm dscfm gr/dscf ppm
U. Percent Water Vapo V. Average Molecular Component Water Carbon Dioxide Carbon Monoxide Oxygen Nitrogen & Inerts FLOW RATE W. Gas Density Correct X. Velocity Pressure C Y. Corrected Velocity (Z. Flow Rate (Y x G x & AA. Flow Rate (Standal BB. Dry Flow Rate (AA SAMPLE CONCENTRA CC. Sample Concentra DD. Sample Concentra	0.015 0.00040 0.20900 0.791 ction Factor (2 orrection Factor (2 o	Dry Basis Ory Basis Ory Basis Dry Basis Ory Basis Ory Basis Dry Basis Ory Basis	Moist. F 1.000 0.985 0.985 0.985 0.985	ract. x	18.0 44.0 28.0 32.0 28.2	, , , , Sum	= W 0.27 0.02 0.00 6.59 21.97 28.84 1.00 1.00 #DIV/0! #DIV/0! #DIV/0! #DIV/0! 5.992E-08 3.24E-05 1.371E+02 #DIV/0!	fps cfm scfm dscfm gr/dscf ppm ng/m3

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APPENDICES

Appendix A: Field Data

		Si A	TO SHARE STATE OF THE SHARE STAT				Quality M					j	- /		
	Te Sa	st No.	17-340 Location:	Cor	mpany:	CAR 431	LTON	FORS	E	D	ate: ample T	5/18	7/17		
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	Fil Pr	ter: _ obe: _	Leak Check: cfm @ cfm @ cfm @ cfm @ cfm @	15	9			Po Filt Pro	st-Test I ter: obe: ot Tube	0	cfm @ _cfm @ _	/S Pass /	_ "Hg \ _ "Hg \ Fail	/ac /ac	
	ime 3:27	Sample Point #	Gas Meter Reading (dcf)	Sta Velocity Head	Temp.	Velocity (fps)	Calculated Sampling Rate	Orifice △P	Probe Temp. °F	Filter Temp. °F	Imp. Temp. °F		Temp. F	Vacuum " Hg	
712	9	<u> </u>	Start: 346.99	("H₂O)	-	31-2	(cfm)	("H ₂ O)	F	Г	the same of the same of	- 000000	10000000		
715	30	7	360.33		0.000			2.9			52	87	89	14	
70	15		38 7,73					3.0			40	97	93	1410	- 4
+	60		401,565			0.00		3.0			47	108	96	15	, ,
2/1	4.27		1010								-	700			
												- 400			
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				100										Barrell La	
	2010-201											08.007.007.00			
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									Traff.						
(N	let Vol	Uncorr.)		Avg.										-	
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No Ba	ozzle arome atic P	Diamet tric Pre ressure	er: 0,50 essure: 2 e in Stack: +	9.89		HgA " I	Re Pit H₂O	ecorded tot Facto	By: or:	2	SA			li .	
			Calibration D				***************************************	A					_	1	
Ma	agneh	elic No	neter No7/	4 (Cal:)				N	diam.	Stac	k ensions	
Po	tentic	meter	No. NO 3/4	/ (Cal: 3	124/17)					diam.	20.007.00	/ ₁	
Th Ga Me	ermo as Me eter C	couple ter No. orr. Fa	No. <u>No 3/4</u> No. <u>No 7/4</u> ctor: /-	(1 (1 	Cal: <u>'</u> Cal: <u>3</u>	124/17)		-	→	<u> </u>	-(1]	
Sa			e: Stainless St				10-		Too .	ontal / Ve			ngular / (
	FUF	NACE	e Temp 15	(7/	SP	1875-	125	VE) +n.	NA		0.000			

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Appendix B: District Laboratory Data/Result

			ALITY MANAGEMENT DIS Diamond Bar, CA 91765-418 Page 1 of 2	
	RE		RING & ANALYSIS ABORATORY ANALYSIS	
TO Mike Garibay			LABORATORY NO	1713606
Supervising A.0				
Source Test & I	Engineering		SOURCE TEST NO	17-340
SAMPLE(S) DESCR			DATE RECEIVED	05/19/17
2 Hexavalent C	hromium Train	S	RULE NO	21.4
SAMPLING LOCAT	CION		RULE NO	NA
Facility ID 229			REQUESTED BY	Eric Padilla
Carlton Forge	•		ALQUESTED BY	Eric Padilla
7743 Adams St.			DATE ANALYZED	05/19/17
Paramount, CA	90723		DATE REPORTED	6/9/2017
			ED, METHOD OF ANALYSI	
Moisture and			CARB 425 (Sodium Bicarbon:	ate(NaHCO3) solution)
Moisture gain, g	Train 49 0.2	Train 50		
Silica gel% expended	0.01	0.8		
Filter gain, g	-0.0013	0.0004		
Impinger 1 pH	9	9		
Impinger 2 pH	9	9		
Cr ⁺⁶ total ug	0.00	0.20		
CI WILL UK	0.16	1.44		
Cr 53 total ug				
	nk remained in	the truck durin	ng the source test.	
Cr 53 total ug Recovery Notes:			ation purposes.	
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the series of the seri	cant figures prov	rided for calcula	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the series of the seri	cant figures prov	rided for calcula	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the field blan Reviewed By: Joan Nic Laborate Approved By:	cant figures prov	A.Q. Chemist	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the field blan Reviewed By: Joan Nic Laborate Approved By: Aaron K	ertit, Principal A	A.Q. Chemist	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the field blan Reviewed By: Joan Nic Laborate Approved By: Aaron K Senior M	ecant figures provertit, Principal Apry Services	A.Q. Chemist	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the field blan Reviewed By: Joan Nic Laborate Approved By: Aaron K Senior M	cant figures provertit, Principal Apry Services	A.Q. Chemist	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the field blan Reviewed By: Joan Nie Laborate Approved By: Senior M Laborate	cant figures provertit, Principal Apry Services	A.Q. Chemist	ation purposes.	06/09/17
Cr 53 total ug Recovery Notes: Train 49: The field blan NOTE: Additional signification of the field blan Reviewed By: Joan Nie Laborate Approved By: Senior M Laborate	cant figures provertit, Principal Apry Services	A.Q. Chemist	ation purposes.	06/09/17

SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT 21865 Copley Dr., Diamond Bar, CA 91765-4182 Page 2 of 2

MONITORING & ANALYSIS REPORT OF LABORATORY ANALYSIS

LABORATORY NO 1713606

REQUESTED BY Eric Padilla

ANALYTICAL WORK PERFORMED, METHOD OF ANALYSIS AND RESULTS Moisture and Hexavalent Chromium by CARB 425 (Sodium Bicarbonate(NaHCO3) solution)

QUALITY CONTROL

BALANCE CHECK

Lab No.	Result (g)	Limit (g)	Check Status
B17E125-CCV1	100	±0.0005	Pass
B17E125-CCV2	500.0	±0.2	Pass

CCV RECOVERIES

Lab No.	Results (ppt)	Limit (%)	% Recovery
S17E058-CCV1	102	90-110	102
S17E058-CCV2	98	90-110	98
S17E058-CCV3	103	90-110	103

REF B17E125 S17E058

Test No. <u>17-340</u> 16 Date: <u>5/18/2017</u>

		RCE TEST REQUEST			
Company		on Forge	Source To	est No.	17-340
Address		Paramount, CA 90723	and the same of th		5/12/17
Basic Equipment		Area - Ambient	Control D	-	N/A
Analysis/Equipment Requ		Eric Padilla	Date Equ	ipment Needed	5/18/17
For Compliance, Rule(s)				
Other (specify)		Rule Development		Facility ID No.	22911
Dry Ice Needed (100 POUNDS)					36 06
Equipment	Requested/ID #	SAMPLE EQUIPMEN			C → T
Two CARB 425 trains	s (NaHCO3 with back	-end		s Requested te, Cr6, moisture	Set I
	ilter)	17.	7 110 =	۵	
00 00 00 00 00 00 00 00 00 00 00 00 00		Train 1		<i>U</i>	137 :
Electric Control of the Control of t		Raferer	rea: Blue Bo	ok No41 Pa	ges 136, 137
Tubing fts	vo 8" sections)	Ta. 21. 40	Tal . ov Cal	I i. b. (A.	Omend
r nonig (tw	o o accuons)	Train 49:	DIAVIK ISTAY	a in truckly	opnous, notulaing
		יטכי משמין:	tulaing, prov	oe, train t	firmace)
Recovery Train 491-01 Train 506-01 Frip Blank):Containe 1):Containe (-08)	r 2 (-02), (cor 1 (-05), (c	ontainer 3 ontainer 2		Hauner 3 (-07
Recovery Train 491-01 Train 50 Ca Trip Blank):Containe t):Containe -08)	r 2 (-02), (c r 1 (-05), (c			Hauner 3 (co7
Frip Blank I	4):Containe (-08)	2 (-02), (c x 1 (-05), (c	T CHAIN OF CUST For (S/T, Analysis	ODY	Hauner 3 (co7
Frip Blank I	4):Containe (-08)	x 1 (-05), (a	T CHAIN OF CUST	ODY	Hauner 3 607
Frip Blank I	4):Containe (-08)	x 1 (-05), (a	T CHAIN OF CUST For (S/T, Analysis Clearyp, Not Used	ODY	
Sample Equipment Set ID Frain's 41,50 Flora	4):Containe (-08)	x 1 (-05), (a	T CHAIN OF CUST For (S/T, Analysis Cleanyp, Not Used S/T Recovery	ODY	
Frip Blank I	4):Containe (-08)	x 1 (-05), (a	T CHAIN OF CUST For (S/T, Analysis Clearyp, Not Used	ODY	
Sample Equipment Set ID Frain's 41,50 Flora	4):Containe (-08)	x 1 (-05), (a	T CHAIN OF CUST For (S/T, Analysis Cleanyp, Not Used S/T Recovery	ODY	
Sample Equipment Set ID Frain's 41,50 Flora	4):Containe (-08)	x 1 (-05), (a	T CHAIN OF CUST For (S/T, Analysis Cleanyp, Not Used S/T Recovery	ODY	

Test No. <u>17-340</u> Date: <u>5/18/2017</u>

Appendix C: Equipment Calibrations

Field Met Ref. Ther Temperatu	mometer	# : <u>NO</u> # : <u>NS</u> e(s): <u>Jo</u>	314 + 1 TM 08- TA FURNAC	10315 343 E		C	alibra Sei	tion tion Pe miannua imonth	te:3-24-17 By: 4/5 =riod: a1 ×
		Λ	10314			No	315	Otne	er
		Lea STQC#	d Wire	_		Lead STQC#	Wire] "
Temp.*	A	В		1)100	1	В	(B-A	1)100	
Sensor Re	ef.	1 Ch#2	Ch#1	** Ch#2	Ch#1	Ch#2	Ch#1	** Ch#2	
10102 2	2 3				32	32	CII#I	Cn#2	COMMENTS
20108 3	3 3:				33	33			
50111 3	3 3	3 33			33	33			
20202 3	3 3	3 33			33	33			
00112 3	3 32	33			33	32			
1 . (15									
10102 2					212				
50111 2	.	1			211	211			
7-11-	2 212				211	211			
	2 21				2/2	212			
01100		1011			4	6/1			
10/02 61	2 61	1612			611	611			
20108 61		1			612	611			
10111 61		611				612			
0202 61	1 611	611				612			
11261	2 612	-611			612				
			,,						
1		1 . 1							

Test No. <u>17-340</u> 18 Date: <u>5/18/2017</u>

ω	N	ь	ω	N	ц	ω	N	ч	ω	N	ь		TRIAL CFM	STAND.	PBAR:	AMBIE	DATE:	
₽	Р	Ľ	3/4	3/4	3/4	1/2	1/2	1/2	1/4	1/4	1/4		CFM	ARD DI		AMBIENT AIR		
6.5	7.0	5.2	4.9	5.1	3.8	2.9	11.5	4.7	1.3	1.1	1.6	cubicF	TOTAL TEMP	STANDARD DRY GAS METER ID#:	29.87	R 74 0	March	
74	74	74	74	74	74	74	74	74	74	74	74		TEMP	ETER ID:	In.Hg	면 면	March 24, 2017	
9	9	9	5.2	5.2	5.2	2.8	2.8	2.8	1.2	1.2	1.2		H2O F	#				
9	9	9	5.2	5.2	5.2	2.8	2.8	2.8	1.2	1.2	1.2		H2O PRESSURE					
9.0	9.0	9.0	5.2	5.2	5.2	2.8	2.8	2.8	1.2	1.2	1.2		RE H20	7812470				DR
399.0	391.7	386.3	379.8	374.4	370.4	366.2	354.6	349.3	346.4	345.2	343.2	(in	M READ1	0				Y GAS ME
405.5	398.7	391.5	384.7	379.5	374.2	369.1	366.1	354.0	347.7	346.3	344.8	(in cubic F)	METER READ1 READ2					TER CA
	7.0		4.9		3.8	2.9	11.5	4.7	1.3	1.1	1.6		TOTAL		DRY GAS			DRY GAS METER CALIBRATION WORKSHEET
													HRS		DRY GAS METER ID		PERFORMED BY:	N WORKS
Q	0	ഗ	O	9	4	υı	21	œ	4	ω	ហ		MIN		ID		ED BY	HEET
25.00	56.00	9.00	14.00	30.00	53.00	18.00	46.00	51.00	7.00	29.00	3.00		SEC				••	н
6.42	6.93	5.15	6.23	6.50	4.88	5.30	21.77	8.85	4.12	3.48	5.05	Decimal	TIME		N0714		W. Stredwick	
1.0130	1.0096	1.0097	0.7861	0.7846	0.7782	0.5472	0.5283	0.5311	0.3158	0.3158	0.3168	CFM	UC FL RT				ick	Page 1

Test No. <u>17-340</u> 19 Date: <u>5/18/2017</u>

9.0 3.1 6.1 859.5 9.0 3.1 6.1 866.5	3/4 4.0 74 5.2 2.0 3.6 837.4 3/4 5.2 74 5.2 2.0 3.6 841.6 3/4 4.8 74 5.2 2.0 3.6 847.0 1 5.4 74 9.0 3.1 6.1 853.4	TRIAL CFM TOTAL TEMP IN OUT H20 READ1 READ2 cubicF 1 1/4 1.7 74 1.2 0.4 0.8 810.0 811.7 2 1/4 1.2 74 1.2 0.4 0.8 812.0 813.2 3 1/4 1.2 74 1.2 0.4 0.8 812.0 813.2 3 1/4 1.2 74 1.2 0.4 0.8 812.0 813.2 3 1/4 1.2 74 1.2 0.4 0.8 812.0 813.2 3 1/4 1.2 74 1.2 0.4 0.8 813.4 814.6 2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1	DATE: March 24, 2017 DRY GAS METER ID : N0714
6.7 6 6.3 6		CubicF HRS MIN 1.7 5 1.2 3 1.2 3 1.2 3 1.2 3	SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT DRY GAS METER CALIBRATION WORKSHEET
.00 6.18 .00 6.18 March 24, 20	5.10 6.60 6.08	SEC TIME UC FL RT Decimal CFM 20.00 5.33 0.3188 48.00 3.80 0.3158 46.00 3.77 0.3186 13.00 9.22 0.5316 50.00 21.83 0.5267 29.00 5.48 0.5289	Page 2 W. Stredwick

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OUTH COAS N	METER	SOUTH COAST AIR QUALITY MANAGEMENT D: DRY GAS METER CALIBRATION WORKSHEET	TION	WORKS	SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT DRY GAS METER CALIBRATION WORKSHEET	н				DATE : PERFORMED BY:	ВҮ:	Page 3 March 24, 20 W. Stredwick
RY GAS N	METER	DRY GAS METER COEFFICIENT CALCULATIONS	ENT	CALCUL	ATIONS							
TANDARD	DRY	STANDARD DRY GAS METER ID#: With Coefficient of	ID#:		7812470 1.0000	DRY	GAS 1	DRY GAS METER N0714	N0714			
TRIAL C	CFM	U/C FlowRate	TEMP	H20	H2O Corrected FlowRate	U/ TEMP FlowRate	TEMP	H20	H20 Corrected FlowRate	COEF	AVE:	
	1/4	0.3168	74	1.2	0.3089	0.3188	74	0.8	0.3105	0.9950	0.9960	
3 2	1/4	0.3158	74 74	1.2	0.3079	0.3158	74 74	0.8	0.3076	1.0010		
	1/2	0.5311	74	2.8	0.5198	0.5316	74	1.88	0.5192	1.0012	1.0145	
3 2	1/2	0.5283	74 74	2.8	0.5172	0.5267	74 74	1.88	0.5144	1.0053		
	3/4	0.7782	74	5.2	0.7662	0.7843	74	3.6	0.7692	0.9960	0.9986	
ω ω	3/4	0.7846	74 74	5.2	0.7725	0.7879	74 74	3.6	0.7727	1.0002		
н	Н	1.0097	74	9	1.0033	1.0157	74	6.05	1.0021	1.0012	1.0006	
ωκ	PF	1.0130	74	6 6	1.0032	1.0177	74	6.05	1.0041	1.0013		
									CORRECTION FACTOR:	FACTOR:		