SOURCE TEST REPORT

17-336

CONDUCTED AT

Mattco Forge 16443 Minnesota Avenue Paramount, CA 90723

HEXAVALENT CHROMIUM EMISSIONS FROM FURNACE #17 & GRINDING AREA

TESTED: March 29, 2017

ISSUED: June 2, 2017

REPORTED BY: P. Eric Padilla

Air Quality Engineer II

REVIEWED BY:

Michael Garibay

Supervising Air Quality Engineer

SOURCE TEST ENGINEERING BRANCH

MONITORING & ANALYSIS DIVISION

Cleaning the air that we breathe...

Test Nos. <u>17-336</u> -2- Date: <u>3/29/2017</u>

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Test Nos. <u>17-336</u> -3- Date: <u>3/29/2017</u>

SUMMARY

a.	Firm	. Mattco Forge
		16443 Minnesota Avenue,
b.	Test Location	
c.	Unit Tested	. Furnace #17 & Grinding Area
d.	Test Requested by	Matt Miyasato (DEO), (909) 396-3249, . <u>SCAQMD</u>
e.	Reason for Test Request	. High ambient air monitor readings of Cr (VI)
f.	Date of Test	. March 29, 2017
g.	Source Test Performed by	Mike Garibay, Wayne Stredwick . Bill Welch, Eric Padilla
h.	Test Arrangements Made Through	Jon Lindbeck (President/General Manager, . Mattco Forge) (562) 634-8635
		Jon Lindbeck, Rob Lewis (Vice President,
g.	Source Test Observed by	Mattco Forge), Tony Garcia (Advanced . Environmental Compliance)
j.	Company I.D. No.	. 181199
k.	Permit No.	. <u>N/A</u>

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RESULTS

Summary of Test Conditions:

During the source test, Furnace #17 was operating at 2050° F. The composition of the nine parts inside the furnace contained 15.53% chromium. In the grinding area, all three grinding stations were being used to process stainless steel parts. The stainless steel being ground contained 17.69% chromium. Due to the nature and configuration of the process, testing was performed as a screening test, non-isokinetically, lacking sampling ports to determine exhaust rate.

Two ambient monitors are located in close proximity to the facility, Monitor 21 and Monitor 23. The map in Figure 1 displays the locations. Table 2 contains monitor results for three different days recent to the test date.

Results:

Table 1, Hexavalent Chromium Emisisons

March 29, 2017

Emissions Source	Concentration (ng/m³) *
Furnace #17	2080
Grinding Area	442

^{*} The concentrations are reported in the same units as the recent ambient air monitoring data (see Table 2).

Table 2, Recent Ambient Air Monitoring Data (ng/m³)

Date	Monitor 21	Monitor 23
3/20/17	1.14	3.05
3/26/17	0.12	0.32
3/29/17	0.24	1.06

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EXECUTIVE SUMMARY

Source testing was conducted at Mattco Forge to identify the specific causes of elevated ambient hexavalent chromium levels measured recently very near to the facility. Furnace #17 and the grinding area were tested to determine if they were potential sources of the elevated ambient readings.

Both the furnace and grinding operations resulted in elevated hexavalent chromium emissions. Notably, the hexavalent chromium emissions from the furnace were 680 times the highest ambient air monitoring reading.

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INTRODUCTION

On March 29, 2017, Engineers from the South Coast Air Quality Management District (SCAQMD) Source Test Engineering (STE) branch conducted source testing at Mattco Forge, Inc. in Paramount, California. The purpose of the testing was to identify the specific causes of elevated ambient hexavalent chromium levels measured very near to the facility.

Operations at the facility were identified as processing chromium-containing materials. It is possible that the processing of these materials could cause hexavalent chromium emissions. The two potential sources that were tested were Furnace #17 and the grinding area.

According to the facility, the material in Furnace #17 contained 15.53% chromium. Nine parts, approximately 55 square inches in surface area each, were being heated in the furnace during testing. The stainless steel parts being ground contained 17.69% chromium.

Sources whose emissions are measured as greater than that of the downwind monitor are considered to be potential contributors to the hexavalent chromium measured by the monitor, with those exhibiting the greater concentrations more positively identified as contributors.

EQUIPMENT AND PROCESS DESCRIPTION

Mattco Forge, Incorporated performs heat treating of stainless steel and non-stainless steel parts for the aerospace industry. Parts are heated in forge furnaces to a specified temperature endpoint dependent upon the product and are then subjected to presses to shape them to meet specific product parameters. Grinding is carried out to remove imperfections and to finish the product cycle.

Furnaces and presses are arranged so that heated parts may be removed at their appropriate temperature and shaped in an expedient manner. Testing was performed only on the heating process and the grinding process.

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SAMPLING AND ANALYTICAL PROCEDURES

Three sampling trains were utilized during testing. Train #10 was used for the testing of Furnace #17, Train #11 was used for the grinding area, and Train #18 was used as a blank sample.

The furnace did not have a stack, but instead had an outlet for the hot air controlled by a damper. The sampling probe was secured with the nozzle facing into the damper opening to collect emissions from the furnace as they were emitted into the atmosphere. Care was taken to prevent the probe from being stuck by the movement of the damper or for interfering with that movement. Because of the lack of a suitable stack, the testing was performed non-isokinetically.

The grinding area is largely enclosed, with a roof ridge vent above and a large roll-up door that is kept closed during grinding operations. The roof ridge vent is designed to allow hot air inside the building to vent to the atmosphere. During the test, the inlet tubing and nozzle were secured to a ladder above the grinding activities and the roll-up door was closed.

Hexavalent Chromium Sampling

Testing was conducted based on California Air Resources Board Method 425 applied to the furnace exhaust and the grinding area, with the procedures of the method specific to stack sampling omitted. Two samples were taken at single non-isokinetic sample points as described above for informational purposes. A third sampling train was used as a blank. Each sampling train consisted of a sampling line, which was used to draw the stack sample from the source. The furnace sample used a quartz probe and nozzle. The sample was then drawn through two impingers each filled with an aqueous solution of 0.1N NaHCO₃ (per Section 21.2), an empty impinger, a 2" filter, and an impinger bubbler filled with tared silica gel. Each sampling train was connected to a leak free vacuum pump, a dry gas meter, and a calibrated orifice. The impingers were contained in an ice bath to condense water vapor and other condensable matter present in the sample stream (see Figure 2).

The samples were extracted using the sampling trains. The pH of the solution in the first impinger was measured after the test, but prior to recovery, at pH of at least 9 (the method requires a pH of 8.0 or higher). The impinger solutions were recovered within 24 hours and the SCAQMD laboratory analyzed the hexavalent chromium in the samples by CARB SOP MLD039. Hexavalent chromium deposited in the filter, sample line and impingers were extracted and analyzed by an Ion Chromatograph equipped with a post-column reactor (IC/PCR) and a visible wavelength detector. Moisture content was determined gravimetrically and volumetrically.

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DISCUSSION/TEST CRITIQUE

For purposes of interpreting the test results, the typical ambient Los Angeles Basin average for hexavalent chromium measured during the most recent SCAQMD Multiple Air Toxics Exposure Study (MATES) IV study is less than 0.1 ng/m³. While all of the results are substantially higher than the background, it should be noted that it takes a significant volume of air at source concentrations substantially higher than the background to affect the ambient air levels. Ambient air levels measured at the monitors are also a function of distance away from the facility, due to air dilution, deposition, and meteorology. The intent of this test was to identify sources that are at least several times higher than the background levels to identify the major contributors and to provide a focus for potential remediation. The average ambient concentration adjacent to the facility was 0.99 ng/m³ for the period surrounding the test date, as compared to the measured source concentrations from the facility, which were 2080 ng/m³ and 442 ng/m³ for the furnace and the grinding area, respectively. These elevated source concentrations are considered to indicate that the facility is contributing to the nearby elevated ambient concentrations.

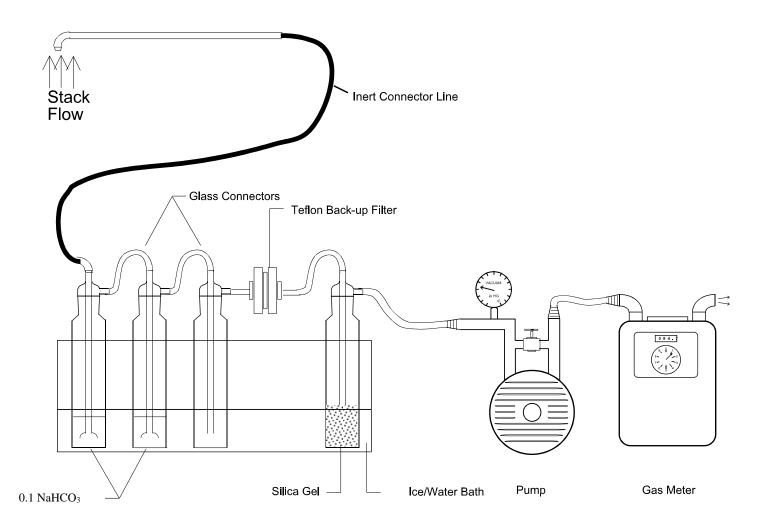
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Figure 1: Facility and Ambient Monitor Location



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Figure 2: CARB Method 425 Train Diagram



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CHROMIUM CALCULATIONS

SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT 21865 E. Copley Dr. Diamond Bar, California 91765-4182

Test No. 2			Test Date: 3/29/17						
	S0	DURCE TES	T CALCULATIONS						
Sampling Location: Sample Train:	Mattco Forge - Furnac 10	e 17		Input I	oy: E. Padilla				
SUMMARY									
	elocity					fps			
	ure (Use 60 deg.F for Te		,			deg F			
	n Factor								
	ssure					"H ₂ 0			
Nozzle Diameter						inch			
1. Stack Diameter or D	Dimension #1	inch	M. Pitot Correction F	actor	0.84				
2. Stack Dim #2 (blank	k if circular)	inch	N. Sampling Time		180	min			
6. Stack Cross Sect. Ar	rea 0.000	ft2	O. Nozzle X-Sect. Ar	ea	0.00000	ft2			
I. Average Stack Temp	#DIV/0!	deg F	P. Net Sample Collec	tion	0.00439	mg			
Barometric Pressure		"HgA	Q. Net Solid Collection			-			
. Gas Meter Pressure ("HgA	R. Water Vapor Cond						
Static Pressure		"H ₂ 0	S. Gas Volume Mete	red	80.679				
. Total Stack Pressure	(I+(K/13.6)) 30.05	"HgA	S2. Amp-hr			amp-h			
. Corrected Gas Volum	ne [(S x J/29.92) x 520/(4	60+B) x C			74.519	dscf			
•	or in Gas Sample ((4.64 x	R)/((0.0464	x R) + T))		3.43	%			
/. Average Molecular				ecular Wt.	3.43				
/. Average Molecular	Weight (Wet):		Fract. x Mo 18	ecular Wt. 	= Wt./l				
Average Molecular Component Vater Carbon Dioxide	Vol. Fract. 0.034 0.00040 Dry Basis	x Moist. F 1.000 0.966	Fract. x Mo 18	ecular Wt. .0 , .0 ,	= Wt./l				
Average Molecular omponent Vater arbon Dioxide arbon Monoxide	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis	x Moist. F 1.000 0.966 0.966	Fract. x Mo 18 44 28	ecular Wt. .0 , .0 ,	= Wt./I				
Average Molecular component Vater arbon Dioxide arbon Monoxide xygen	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966	Fract. x Mo 	ecular Wt. .0 , .0 , .0 ,	= Wt./I 0.62 0.02 0.00 6.46				
Average Molecular component Vater arbon Dioxide arbon Monoxide xygen	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis	x Moist. F 1.000 0.966 0.966	Fract. x Mo 18 44 28	ecular Wt. .0 , .0 , .0 ,	= Wt./I				
Average Molecular Component Vater Carbon Dioxide Carbon Monoxide	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966	Fract. x Mo 	ecular Wt. .0 , .0 , .0 ,	= Wt./I 0.62 0.02 0.00 6.46				
Average Molecular Component Vater Carbon Dioxide Carbon Monoxide Dixygen Litrogen & Inerts CLOW RATE V. Gas Density Correc	Veight (Wet): Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966	18 44 28 32 28	ecular Wt. 0 , 0 , 0 , 0 , 2 , Sum	= Wt./I 0.62 0.02 0.00 6.46 21.53 28.62				
Average Molecular Component Vater Carbon Dioxide Carbon Monoxide Carbon Monox	Veight (Wet): Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966	Fract. x Mo 18 44 28 32 28	ecular Wt. 0 , 0 , 0 , 0 , 2 , Sum	= Wt./I 0.62 0.02 0.00 6.46 21.53 28.62 1.01	Mole 			
Average Molecular omponent Vater arbon Dioxide arbon Monoxide xygen itrogen & Inerts LOW RATE V. Gas Density Correct Velocity Pressure Co.	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28	0 ,	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0!	Mole fps			
Average Molecular omponent Vater arbon Dioxide arbon Monoxide xygen itrogen & Inerts LOW RATE / Gas Density Correct Velocity (According to the control of the corrected Velocity (According to th	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 322 28	0 ,	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0!	Mole fps cfm			
Average Molecular omponent //ater arbon Dioxide arbon Monoxide xygen itrogen & Inerts LOW RATE // Gas Density Correct	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis o.791 Dry Basis tion Factor (28.95/V)^.5 A x M x W x X)	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28	0 , .0 , .0 , .0 , .2 , Sum	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0!	Mole 			
Average Molecular omponent Vater arbon Dioxide arbon Monoxide xxygen itrogen & Inerts LOW RATE Velocity Pressure Co. Velocity Pressure Co. Corrected Velocity (V. G. Flow Rate (Y x G x 6 A. Flow Rate (Standar	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28	0 , .0 , .0 , .0 , .2 , Sum	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0!	fps cfm scfm			
Average Molecular component Vater Indian Dioxide carbon Monoxide component carbon Monoxide carbon Monoxide component carbon Monoxide component carbon Monoxide carbon Monoxid	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis o.791 Dry Basis tion Factor (28.95/V)^.5 A x M x W x X)	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28	0 , .0 , .0 , .0 , .2 , Sum	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0!	Mole 			
Average Molecular Component Vater Carbon Dioxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Carbo	Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis 0.791 Dry Basis tion Factor (28.95/V)^5. prection Factor (29.92/L) A x M x W x X)	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28	lecular Wt. .0 , .0 , .0 , .0 , .2 , . Sum	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0! #DIV/0!	fps cfm scfm dscfm			
Average Molecular omponent //ater arbon Dioxide arbon Monoxide xygen itrogen & Inerts LOW RATE // Gas Density Correct Velocity Pressure Co. Corrected Velocity (Figure 1988). Flow Rate (Standar B. Dry Flow Rate (AA) AMPLE CONCENTRA C. Sample Concentrate	Veight (Wet): Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis tion Factor (28.95/V)^5.5 prection Factor (29.92/L) A x M x W x X)	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28	ecular Wt. 0 , 0 , 0 , 0 , 2 , Sum	= Wt./I 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0! #DIV/0!	fps cfm scfm dscfm			
Average Molecular omponent Vater arbon Dioxide arbon Monoxide xygen itrogen & Inerts LOW RATE V. Gas Density Corrector Velocity Pressure Corrected Velocity (A. Flow Rate (Standar B. Dry Flow Rate (AA. AMPLE CONCENTRA C. Sample Concentrat D. Sample Concentrat Ample Concentrat D. Sample Concentrat D.	Veight (Wet): Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis tion Factor (28.95/V)^5.5 prection Factor (29.92/L) A x M x W x X)	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28 Wt.)]	ecular Wt. 0 , 0 , 0 , 0 , 2 , Sum	= Wt./I 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0! #DIV/0! #DIV/0!	fps cfm scfm dscfm gr/dscf			
Average Molecular Component Vater Sarbon Dioxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Monoxide Carbon Car	Veight (Wet): Vol. Fract. 0.034 0.00040 Dry Basis Dry Basis 0.20900 Dry Basis 0.791 Dry Basis 0.791 Dry Basis tion Factor (28.95/V)^5.5 prection Factor (29.92/L) A x M x W x X) 0)	x Moist. F 1.000 0.966 0.966 0.966 0.966	18 44 28 32 28 Wt.)].	Sum	= Wt.// 0.62 0.02 0.00 6.46 21.53 28.62 1.01 1.00 #DIV/0! #DIV/0! #DIV/0! 9.090E-07 4.92E-04 2.08014E+03 #DIV/0!	fps cfm scfm dscfm gr/dscf ppm ng/m3 lb/hr			

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SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT 21865 E. Copley Dr. Diamond Bar, California 91765-4182

	lo. 1				Test Date:	3/29/17	
		SOL	JRCE TEST	CALCULATION	S		
Sampling Location: Sample Train:	Mattco For	ge - Grinding	g Area		Input by:	E. Padilla	
SUMMARY							
A. Average Traverse V	elocity					. #DIV/0!	fps
B. Gas Meter Tempera	ture (Use 60 d	eg.F for Ten	np Comp. N	leters)		. 89.7	deg F
C. Gas Meter Correction							
Average Orifice Pres							
Nozzle Diameter							inch
1. Stack Diameter or I	Dimension #1.		. inch	M. Pitot Corre	ction Factor	0.84	
2. Stack Dim #2 (blan	k if circular)		. inch	N. Sampling T	ime	180	min
6. Stack Cross Sect. A	rea	. 0.000	ft2	O. Nozzle X-S	ect. Area	0.00000	ft2
I. Average Stack Tem _l	p	. #DIV/0!	deg F	P. Net Hex Ch	rome Collection	0.00097	mg
Barometric Pressure.			•		e Collection		•
. Gas Meter Pressure					or Condensed		
Static Pressure			"H₂0		e Metered	81.158	
. Total Stack Pressure	∍ (I+(K/13.6))	30.05	"HgA	S2. Amp-hr			amp-h
. Corrected Gas Volur	me [(S x J/29.9	2) x 520/(46	0+B) x C			77.429	dscf
			· ·				
ERCENT MOISTURE	/GAS DENSIT	Y					
 Average Molecular component 		ol. Fract.	c Moist. F	Fract. x	Molecular Wt.	= W	t./Mole
 Vater	0.007		1.000		18.0 .		
Carbon Dioxide						0.12	
	0 00040	Dry Rasis	0 993		•	0.12 0.02	
	0.00040	Dry Basis Dry Basis	0.993 0.993		44.0 ,	0.12 0.02 0.00	
arbon Monoxide		Dry Basis	0.993		•	0.02	
arbon Monoxide xygen	0.20900				44.0 , 28.0 ,	0.02 0.00	
arbon Monoxide xygen	0.20900	Dry Basis Dry Basis	0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 ,	0.02 0.00 6.64 22.15	
Carbon Monoxide Oxygen	0.20900	Dry Basis Dry Basis	0.993 0.993		44.0 , 28.0 , 32.0 ,	0.02 0.00 6.64	
Jarbon Dioxide Daygen Dixygen & Inerts	0.20900	Dry Basis Dry Basis	0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 ,	0.02 0.00 6.64 22.15	
Carbon Monoxide Oxygen litrogen & Inerts	0.20900 0.791	Dry Basis Dry Basis Dry Basis	0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93	
arbon Monoxide bxygen litrogen & Inerts LOW RATE J. Gas Density Correct	0.20900 0.791	Dry Basis Dry Basis Dry Basis	0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93	
arbon Monoxide xygen itrogen & Inerts LOW RATE J. Gas Density Correc Velocity Pressure C Corrected Velocity (0.20900 0.791 ction Factor (20 orrection Factor (A x M x W x X)	Dry Basis Dry Basis Dry Basis Dry Basis	0.993 0.993		44.0 , , 28.0 , 32.0 , , 28.2 , , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0!	fps
arbon Monoxide bygen litrogen & Inerts LOW RATE V. Gas Density Correc Velocity Pressure C Corrected Velocity Flow Rate (Y x G x 6	0.20900 0.791 ction Factor (2/ orrection Fact (A x M x W x X)	Dry Basis Dry Basis Dry Basis Dry Basis	0.993 0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0!	cfm
arbon Monoxide xygen itrogen & Inerts LOW RATE J. Gas Density Correct Velocity Pressure C. Corrected Velocity (Flow Rate (Y x G x & A. Flow Rate (Standar	0.20900 0.791 ction Factor (28 orrection Fact (A x M x W x X) 50)	Dry Basis Dry Basis Dry Basis Dry Basis 8.95/V)^.5 or (29.92/L)^\(0.000)	0.993 0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0!	cfm scfm
arbon Monoxide xygen itrogen & Inerts LOW RATE J. Gas Density Correct Velocity Pressure C. Corrected Velocity (Flow Rate (Y x G x & A. Flow Rate (Standar	0.20900 0.791 ction Factor (28 orrection Factor (A x M x W x X) 50)	Dry Basis Dry Basis Dry Basis Dry Basis 8.95/V)^.5 or (29.92/L)^\(0.000)	0.993 0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0!	cfm scfm
arbon Monoxide xygen itrogen & Inerts LOW RATE /. Gas Density Correc . Velocity Pressure C . Corrected Velocity (. Flow Rate (Y x G x 6 A. Flow Rate (Standal B. Dry Flow Rate (AA	0.20900 0.791 ction Factor (2torrection Factor A x M x W x X) 60)	Dry Basis Dry Basis Dry Basis 3.95/V)^.5 Dr (29.92/L)^.	0.993 0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0!	cfm scfm
arbon Monoxide xygen itrogen & Inerts LOW RATE J. Gas Density Correct. Velocity Pressure C. Corrected Velocity (Flow Rate (Y x G x & A. Flow Rate (Standal B. Dry Flow Rate (AA)	0.20900 0.791 ction Factor (26 orrection Factor) (A x M x W x X) (50)	Dry Basis Dry Basis Dry Basis Dry Basis 8.95/V)^.5 Dr (29.92/L)^	0.993 0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0! #DIV/0!	cfm scfm dscfm
arbon Monoxide ixygen & Inerts LOW RATE I. Gas Density Correct. Velocity Pressure C. Corrected Velocity (Flow Rate (Ystandal B. Dry Flow Rate (AA) AMPLE CONCENTRA C. Sample Concentra D. Sample Concentra D. Sample Concentra	0.20900 0.791 ction Factor (2! orrection Facto A x M x W x X) 600rd) {Z x (L/29.9 x (U/100))rd) tition [0.01543 x) tition [0.01543 x)	Dry Basis Dry Basis Dry Basis Dry Basis 8.95/V)^5 Dr (29.92/L)^6 ON RATE ((P/T)] 100	0.993 0.993 0.993		44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0! #DIV/0! 1.933E-07 1.05E-04	cfm scfm dscfm gr/dscf ppm
arbon Monoxide bygen litrogen & Inerts LOW RATE V. Gas Density Correc . Velocity Pressure C . Corrected Velocity (. Flow Rate (Y x G x 6 A. Flow Rate (Standal B. Dry Flow Rate (AA AMPLE CONCENTRA C. Sample Concentra D. Sample Concentra E. Sample Emission F	0.20900 0.791 ction Factor (2/2) orrection Factor A x M x W x X) 50)	Dry Basis Dry Basis Dry Basis Dry Basis Dry Basis 3.95/V)^5	0.993 0.993 0.993	Wt.)]	44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0! #DIV/0! #DIV/0! 1.933E-07 1.05E-04	cfm scfm dscfm gr/dscf ppm ng/m3
carbon Monoxide bxygen litrogen & Inerts LOW RATE	0.20900 0.791 ction Factor (2torrection Factor Ax M x W x X) 50)	Dry Basis Dry Basis Dry Basis Dry Basis 8.95/V)^.5 Dr (29.92/L)^ 0 22) x [520/(44 ON RATE x (P/T)] 100 x BB xCC) Q x BB)/T]	0.993 0.993 0.993	Wt.)]	44.0 , 28.0 , 32.0 , 28.2 , Sum	0.02 0.00 6.64 22.15 28.93 1.00 1.00 #DIV/0! #DIV/0! #DIV/0! 1.933E-07 1.05E-04 4.423E+02 #DIV/0!	cfm scfm dscfm gr/dscf ppm ng/m3 lb/hr

Test No. <u>17-336</u> -13- Date(s): <u>3/29/2017</u>

APPENDICES

Test No. <u>17-336</u> -14- Date(s): <u>3/29/2017</u>

APPENDIX A

Field Data

Т	et No	17-336	Com	nany:	Mai	total	Fores	٤,	Г	ate.	3/29	1,7	
Sa	ampling	17-336 Location:	12400	Bull.	#12	1700	1 7		S	ample T	rain:	11 1	10
			7		Traverse	Source	Test Da	ta					
Pr	e-Test	Leak Check:					Po	st-Test L	eak Ch	eck:			
Fi	Iter:	cfm @ cfm @		"Hg	vac		Filt	er:	(cfm @	- 1	_ "Hg ۱	/ac
Pi	robe: tot Tub	crm @ e Leak Check:	Poss	/ Fail	vac		Pro	obe: (۱ <u>۵۵. ۵</u>	cim @	12	_ "Hg \ Eail	/ac
FI	tot Tube	e Leak Check.	Pass / Fail			Pitot Tube Leak Check:				Pass / Pall			
		Gas Meter	Sta	ck	(Calculated		Probe	Filter	Imp.	Meter	Temp.	Vacuum
	Point #	Reading (dcf)	Velocity Head	Temp.	Velocity (fps)	Sampling Rate	Orifice △P	Temp.	Temp.	Temp.		F	" Hg
		Start:	rread ("H₂O)	-	(ips)	(cfm)	("H ₂ O)	°F	°F	°F	ln		
1103	<u>.</u>	261.866								720	86	84	211
+10		265,75								50		87	311
+20		270,2								45	93		3"
130		274.7								47		91	3/1
140		279.2	→ Hardy Section	CL0993005040						48	99	24	311
150		283.75	140				10.00			50 47	101	95	3"
470		298,255								77	103	100	2
+85		297,280							1	76	106	101	311
190		301,810		- 15-4 6)	49		CONTROL OF SHARE	31
+100			2000 C 10							48	108	103	34
+110		306,350								46			3"
+120		315,375								45	109	105	311
+130	2.0	319.9								51	109	106	3"
4140	COLUMN COLUMN	324.45								55	110	107	311
4150		328.75		32.00				150		53	//0	CHARLEST CONTRACTOR	
+ 160		333-4		19400000000000						54	-/-/	107	3/
t/70		338.6	_						- A-	53	110	107	- 5
+180		342,54	•						- ₺				
												A Color of Bases	
						EXCESSES A STREET		TO THE STATE OF TH					
		10.00											
(1)-4)/-1	11		Avg.								<u> </u>	L	
(Net Vol.	Uncorr.)		- 1										
K-Facto	or:		Stack	Moistu	re:	C	anister #	t:		Star	t:	"	∃g vac
Nozzle	Diamet	er.	"			R	ecorded	Bv:	BW	(1ch			
Barome	etric Pre	essure: 2	30,01	5 "	HaA	Pi	tot Facto		W.	OCO V			
Static F	Pressure	essure: 2 e in Stack: +	1-		"	H₂O						$\overline{}$	
							1	_		√	\rightarrow	_/	
Inclina	d Manar	Calibration D neter	ala (Cal: _	N/A	\				N	diam.		
Magne	a Manor helic No		(oai. Cal·	11//	'		1	1		X		
Pitot Ti	ihe No).	— ;	Cal:		í l	١,	1	Λ		•	Sta	
Potenti	ometer	No. NO319	5 (-73-17	í l	↓				diam.	Din	nensions
Thermo	ocouple	No.		Cal:		j		l			<u>,</u> ,	1	
		NUT 15	(Cal:		j			-		- 1	<u></u>	7
Meter C	Corr. Fa	ctor: 0,9			3/23/								
		e: Stainless St					Stack	r: Horiz	zontal / Ve	ertical	Rects	ıngular /	Circular
Sambiii	ייטי ו טוי						Otaci				1 (000		

Test No. <u>17-336</u> -15- Date(s): <u>3/29/2017</u>

Te	st No.	<u>17-336</u> Location:	Con	npany:	M	attec	Fol	90	D	ate:	3/29	1/17	,
Sa	ampling	Location:	Grin	ding	Area	1			S	ample T	rain:	11	
D-	- T4	Laste Obaste		0	Traverse	Source	Test Da	ta Tool I	eak Che				
Fil	e-Testi ter	Leak Check: cfm @)	"Ho	vac							"Ha v	/ac
Pr	obe:	cfm @	12	— ;;;	vac			bbe:	0	rfm @ _	15	"Hg \	ac
Pit	tot Tube	Leak Check:	Pass	/ Fail			Pite	ot Tube	Leak Ch	eck:	Pass /	Fail	
Time	Sample	Gas Meter	T Sta	ıck	,	Calculated		Probe	Filter	Imp.	Meter	Temp.	Vacuum
111110	Point #	Reading (dcf)	Velocity	Temp.	Velocity	Sampling	Orifice	Temp.	Temp.			F	" Hg
	. "	Start: 891, 796	Head ("H₂O)	°F	(fps)	Rate (cfm)	∆P ("H₂O)	°F	°F	°F	In	Out	
1ºº AM		818.09	2.60				45			39	74	75	15
+10		898.09	2,15							41	79	75	12
726		906,58	2.15							44	85	78	12
+40		912.79	0.50							30	86	78	12
+50		921.54								3-3	89	82	3
+60		925.53								5-3	89	84	_3
+70		929.48								52	91	86	3
+80		933, 46				1470, 200, 51, 96, 00				54	92	Control Control	3
+90		941, 42	0.49							49	94	90	3
+110			0.49							570	95	90	3
+120		949. 38	0-49							52	96	91	3 .
+130			0.49							5-2	96	92	٨
+ 140			0.49							51	97	92	3
+150		961.16	0.49							53 49	97	93	3
+110			0.49							51	97	93	3
+180		972.954	0.49							53-	98	94	3
		•											
					1								
(Net Vol.		-/	Avg.			l		ı		04		"	
	-	. 5682		Moistu	re:								ng vac
		er: <u>M/A</u> essure:		Б "	НαΔ		ecorded tot Facto		1				
Static P	ressure	e in Stack: +	-1-	MA	' ig∧ " i	H ₂ O	- act	J1.					
		Calibration D		70/11		-2-	—		_	↑	\rightarrow	_/	
nclined		neter		Cal:	N/A)				N 1	diam.		
	nelic No			Cal:))			b _	
Pitot Tu	be No.	-	(Cal: _)	1 1			٦		314	ek nensions
	ometer			Cal: 🔫	124/17)	•	\rightarrow	-		diam.		
i hermo Gas Me	couple ter No	No. No. 714		Cal: Cal: _3	124/12	(-		-	→	7	<u> </u>	کے/	7
	orr. Fa			Oai	124/17	'			l			<u></u>	

Test No. <u>17-336</u> -16-Date(s): 3/29/2017

APPENDIX B

District Laboratory Data

SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT

		ONITORING & A Γ OF LABORATO		
TO Mike Garibay			LABORATORY NO	1708210
Supervising A.C Source Test & E	` •		SOURCE TEST NO	17-336
SAMPLE(S) DESCR			DATE RECEIVED	03/30/17
3 Hexavalent Cl	hromium Trains		RULE NO	NA NA
SAMPLING LOCAT			REQUESTED BY	Wayne Stredwick
Facility ID 1811 Mattco Forge 7530 Jackson St			DATE ANALYZED	3/30/2017
Paramount, CA	90723			
			IOD OF ANALYSIS ANI (Sodium Bicarbonate(Na	
	TRAIN 11	TRAIN 18	TRAIN 10	
Moisture gain, g	11	1.2	57	
Silica gel% expended	95	0	95	
•	95 0.0027	0 -0.0007	95 0.0004	*
Filter gain, g		-		+
Filter gain, g Impinger 1 pH	0.0027	-0.0007	0.0004	*
Filter gain, g Impinger 1 pH Impinger 2 pH	0.0027 9-10	-0.0007 9	0.0004 9	
Filter gain, g	0.0027 9-10	-0.0007 9 9	0.0004 9 9	
Filter gain, g Impinger 1 pH Impinger 2 pH	0.0027 9-10 9-10	-0.0007 9 9 Field Blank, No Tubing,	0.0004 9 9	
Filter gain, g Impinger 1 pH Impinger 2 pH Recovery notes Cr ⁺⁶ total ug NOTE (1) Additional s Reviewed By:	0.0027 9-10 9-10 Tubing Only 0.97	-0.0007 9 9 Field Blank, No Tubing, No Probe 0.00 provided for calcula	0.0004 9 9 Probe & Tubing 4.39	04/14/17 4/14/17

Test No. <u>17-336</u> -17- Date(s): <u>3/29/2017</u>

SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT 21865 Copley Dr., Diamond Bar, CA 91765-4182 Page 2 of 2

MONITORING & ANALYSIS REPORT OF LABORATORY ANALYSIS

LABORATORY NO1708210REQUESTED BYWayne Stredwick

ANALYTICAL WORK PERFORMED, METHOD OF ANALYSIS AND RESULTS Moisture and Hexavalent Chromium by CARB 425 (Sodium Bicarbonate(NaHCO3) solution)

QUALITY CONTROL

BALANCE CHECK

Lab No.	Result (g)	Limit (g)	Check Status
B17D007-CCV1	99.9999	±0.0005	Pass
B17D007-CCV2	500.0	±0.2	Pass

CCV RECOVERIES

Lab No.	Results (ppt)	Limit (%)	% Recovery
S17D005-CCV1	102	90-110	102
S17D005-CCV2	95	90-110	95
S17D005-CCV3	97	90-110	97
S17D005-CCV4	97	90-110	97
S17D005-CCV5	99	90-110	99
S17D005-CCV6	98	90-110	98

REF B17D007 S17D005

Test No. <u>17-336</u> -18- Date(s): <u>3/29/2017</u>

Camman		CE TEST REQUEST			17 224	
Company		o Forge	Source T		17-336 March 23, 2017	
Address Basic Equipment	/330 Jackson Street,	Paramount, CA 90723	Request I		March 23, 2017	
Analysis/Equipment Ro	ouested By	Wayne Stredwick		ipment Needed	March 28, 201	7
For Compliance, Rule						
Other (specify)		Rule Development		Facility ID No.	181199	
Dry Ice Needed 13/ 03/28	it .	SAMPLE EQUIPMEN		ooratory No.	1708210	
Equipmen	t Requested/ID #	Man Do Equi ma		is Requested		Set ID
3 A-Ca	rb 425 Trains		Vos. 10,	11.18.		
(Use sodium bicarbo	nate solution and back fi	iter) Referen	ce: Blue	Book Pages	No125, 12	6.
				41		
A 10 A						
. 19.		*18: Held	Blank (no.	tulaing)		
		*11: tub	ing	J		
and the second s		*10 stubi	ng + probe			
en e	ing the second single consequence of the first of the first of the second o		J. Lapro	dae not cupplie	d by lab.	
			STa	ulready had s	mobe	
					AS 03/30/11	
		1				
	1.4					
1	gridle:					
	S	AMPLE EQUIPMEN	CHAIN OF CUST			
Sample Equipment	From	То	Cleanup, Not Use			
Sample Equipment Set ID	A	Wast.	<u> </u>	3-28-17	7 /2.'57	
Sample Equipment Set ID 0, 11, 18	mionimoun	Plet and the War.	Analysis	03/30/17	07:50	
Sample Equipment Set ID 0,11,18 0,14,18	www.moen	MUMONIAL		04/03/17	13:00	1
Sample Equipment Set ID 0, 11, 19 0, 14, 18 0, 11, 18	inwonsamelh	Saga Root	Analysis	01/03/11		
Sample Equipment Set 1D 0, 11, 18 0, 14, 18 0, 11, 18	inwonsamely	Sugar Rost	Analysis	01/03/17		
Sample Equipment Set 1D 0, 11, 18 0, 14, 18 0, 11, 18	inwansamelh	Swager Right	Analysis	01/05/17		

Test No. <u>17-336</u> -19- Date(s): <u>3/29/2017</u>

APPENDIX C

Equipment Calibrations

	2017																			
Page 3	March 24, 2017			OVERALL	1.0024				1.0024											
				AVE	0.9960	1.0145	1,0369 0,9960 0,997 1,0002 1,0002 0,9931 1,0013 1,0013	1.0006												
	DATK : PERFORMED BY:			CORP	0.9950			ACTOR:												
	PES			Time H20 Corrected C	0.3056 0.3076 0	0.5192	0.7572 0	1.0021	CORRECTION											
			. No.7		8 8 8		3.6													
SEMENT DISTRICT			METER I		4 4 4	74 1.86 74 1.88 74 1.86	2 2 2	74 6.05 74 6.05 74 6.05												
			DRY GAS METER ID : NO714	U/C FlowRate	0.3188 0.3158 0.3186	0.5316 0.5267 0.5289	0.7843	1.0157												
									2017											
		TONS	7812470	1.0000 Corrected FlowRate	0.3089	0.5198 0.5172 0.5356	0.7662	1.0033	DRY GAS METER ID : NOT14 DATE: March 24, 2017											
		LCULAT		H20 Co	7 7 7	9 9 9		S MSTR												
TON Y		D THE		TRMP	222	222	* * *	4 4 4	DRY GA											
SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT DRY GAS METER CALIBRATION WORKSHEET		DRY GAS METER COEPFICIENT CALCULATIONS	AS METER	U/C 1	0.3158	0.5283	0.7782	1.0097												
			D DRY	CPM	1,4	1/2	3/4													
			STANDARD DRY DAS METER IDS:	TRIAL	- 0 -	m m m	11 N N	~ ~ ~												
Page 1	×			UC PL RE TRIAL	0.3168	0.5311	0.7846	1.0097	Page 2	×		UC PL RT	0.3188	0.5316	0.7873	1.0157				
	W. Stredwick	30714		TIME	3 . 4 8 . 1 2 8 . 1 2 8	8.85 21.77 5.30	6.80	5.15 6.93 6.42	ά.	W. Stredwick		TIME	3.80	9.22 21.83 5.48	6.60 6.08	5.32 6.58 6.18				
	*				29.00	\$1.00 46.00	30.00	9.00		x		SHC	20.00 48.00	13.00 50.00 29.00	6.00 36.00 5.00	19.00 35.00				
BOUTH COAST AIR GUALITY MANAGEMENT DISTRICT DRY GAS MRTER CALIBRATION PORKSHEET	D BY:			MIN SEC	8 m 4	0 7 9	400	200	TRICE	D BY:		MIN S		2 2 2						
	PERPORME	PERFORMED IN:		HRS					MMNT DIS	PERPORMED BY:										
		DRY GAS		TOTAL	3 6	4 11 2	0 0 4 0 4 6	8 6 6	6.5 MANAGES			Publick	7 2 2	11.5	4 N 4 0 4 8	47.0				
				READI READE 7	344.8	354.0 366.1 369.1	374.2 379.5 384.7	391.5 398.7 405.5	BOUTH COAST ALR QUALITY MANAGEMENT DISTRICT DRY OAS METER CALIBRATON WORDSHIFT			METER READ1 READ2 CubicF HRS (in cubic F)	813.2	821.1 833.0 836.1	841.4 846.8 851.8	858.8 866.2 872.8				
				READ1 (in cu	345.2	349.3 354.6 366.2	370.4	392.7	AOT AIR DAS METE			READ!	812.0	816.2 821.5 833.2	837.4	859.4				
			7812470	H20	2 2 2	9 9 9	4 4 4	0.66	DRY O			H20		1.9	9 9 9	777				
				PRESSURE		0. 0. 0. 0. 0. 0.	444		ă			SSURE	4 4 4	0 0 0	000					
		In.Hg	FRAR: 29.87 In.Hg STANDARD DRY GAS METER ID#:	HZO PI	244	0 0 0 0 0 0	****				4	HZO PRESSURE IN OUT	444	8 8 8	4 44 44	000				
	4, 2017			S.	74 47	4 4 4 4 4 4	4 4 4	4 4 4		4, 2017	4170N	TBMP I	7 4 4 7	2 4 4		2.4.4				
	DATE: March 24, 2017 AMBIRT AIR 74 0 F	29.87		OAS NE	OAS ME	29.87 OAS KE	OAS ME	TOTAL TEMP	1.1	11.5	4.9	9 4 8		March 24, 2017	E E	TOTAL T	1.2	4.9 2.9	0.50	6.74
	2		ARD DRY		1/4	1/2 2	3/4				DRY GAS METER ID		 	1/2 1	3/4	444				
	DATE:	PBAR:	STAID	TRIAL CPM		486				DATE	DRY GA	TRIAL CPM	- 44 -	- 2 5						

Test No. <u>17-336</u> -20- Date(s): <u>3/29/2017</u>

Ref. I	Meter :	eter #	: <u>NO</u> : <u>AC</u> (s) : <u>J</u>	M 08 A FURNA	Calibration By: US Calibration Period: Semiannual Semianthly							
			N	0314			No.	er				
\			Lead STQC#_	l Wire			Lead STQC#]				
Temp.	* A		В		(B-A)100 A **		В	(B-A	1)100			
Senso: STQC#	Ref. Temp.	Ch#1	Ch#2	Ch#1	Ch#2	Ch#1	Ch#2	Ch#1	** Ch#2	COMMENTS		
10102	32	32	32			32	32			COMMENTS		
20108	33	33	33			33	33					
50111	33	33	33			33	33					
20202	33	33	33			33	33					
0112	33	33	33.			33	32					
	211	115	212			212	212					
20108		211	211			211	211					
0111	711	211	211			211	211					
0202	212	215	214				212					
0112	212	211	211			212	211					
0102	612	1011	/13				()					
0108	611	610	612			611	611					
0111	612	611	611			612						
202	611	611	611			612						
	612		611			612				·		
,,,,,			-			*10	011			7.		
										·		